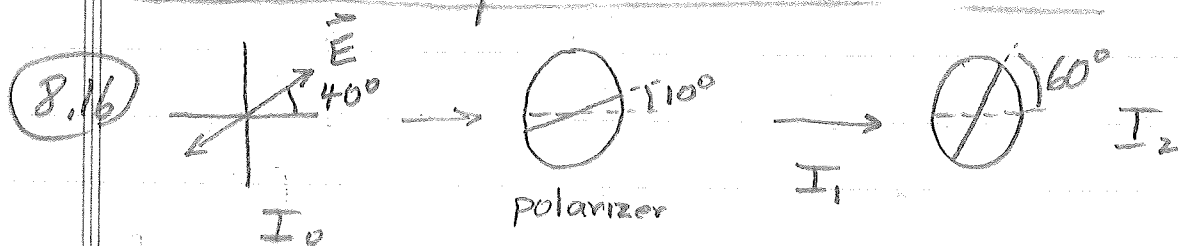


# Physics 302 Photonics

## HW-9 Chapt 8 - SOLUTIONS



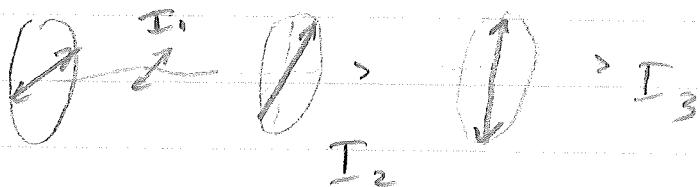
$$\Rightarrow I_1 = I_0 \cos^2(40^\circ - 10^\circ) = 0.75 I_0$$

$I_1$  is at  $\theta_2 = (60^\circ - 10^\circ) = 50^\circ$  wrt. 2<sup>nd</sup> polarizer

$$\Rightarrow I_2 = I_1 \cos^2 \theta_2 = (0.75 I_0) (\cos^2 50^\circ)$$

$$\boxed{I_2 = 0.310 I_0} \text{ ie } \underline{\underline{31\% \text{ emerges}}}$$

8.17 Question should be: "What percentage of light emerges from 2<sup>nd</sup> polarizer?"



$$I_2 = I_1 \cos^2 45^\circ$$

$$I_3 = I_2 \cos^2 45^\circ = I_1 \cos^4 45^\circ$$

$$\boxed{I_3 = 0.25 I_1}, \text{ ie } \underline{\underline{25\% \text{ emerges}}}$$

$$8.32 \quad V = \frac{V_p}{I_p + I_N}$$

$$\text{But } R_{\parallel} = \frac{\tan^2(\theta_i - \theta_t)}{\tan^2(\theta_i + \theta_t)}$$

$$R_{\perp} = \frac{\sin^2(\theta_i - \theta_t)}{\sin^2(\theta_i + \theta_t)}$$

Since incident light is "natural" (unpolarized)

$$I_{\parallel i} = I_{\perp i} = I_0/2$$

(The reflected irradiance is):  $I_{r\parallel} = R_{\parallel} I_{\parallel i} = R_{\parallel} I_0/2$

$$I_{r\perp} = R_{\perp} I_{\perp i} = R_{\perp} I_0/2, \text{ Also } I_{\text{total}} = I_{\parallel i} + I_{\perp i} = I_0$$

So we need to calculate two "V"s:

$$V_{\parallel} = \frac{I_{r\parallel}}{I_{\text{total}}} = \frac{R_{\parallel} I_0/2}{I_0} = \frac{R_{\parallel}}{2}, \text{ and } V_{\perp} = \frac{I_{r\perp}}{I_{\text{total}}} = \frac{R_{\perp} I_0/2}{I_0} = \frac{R_{\perp}}{2}$$

To calculate  $R_{\parallel}$  and  $R_{\perp}$ , we need  $\theta_t$  from Snell's law:

$$1 \sin \theta_i = n \sin \theta_t \Rightarrow \theta_t = \sin^{-1} \left( \frac{\sin \theta_i}{n} \right) = \sin^{-1} \left( \frac{\sin 40^\circ}{1.5} \right) = 25.37^\circ$$

$$\Rightarrow R_{\parallel} = \frac{\tan^2(40^\circ - 25.37^\circ)}{\tan^2(40^\circ + 25.37^\circ)} = \frac{0.06814}{4.756} = 0.0143$$

$$R_{\perp} = \frac{\sin^2(40^\circ - 25.37^\circ)}{\sin^2(40^\circ + 25.37^\circ)} = \frac{0.06379}{0.8263} = 0.0772$$

$$\Rightarrow \boxed{V_{\parallel} = 7.16 \times 10^{-3} \quad \mid \quad V_{\perp} = 0.0386}$$

8.51) From eq. 8.44

$$V_{\frac{\lambda}{2}} = \frac{\lambda_0}{2n_0^3 r_{63}} = \frac{550 \text{ nm}}{2(1.58)^3 (5.5 \times 10^{-12} \frac{\text{m}}{\text{V}})} = 12.8 \text{ kV}$$

8.71)  $E_t = A E_i$  where  $E_i = \begin{pmatrix} E_{ix} \\ E_{iy} \end{pmatrix}$

a) Consider action of  $A_1 = \frac{1}{\sqrt{2}} e^{-i\pi/4} \begin{pmatrix} 1 & i \\ i & 1 \end{pmatrix}$

on various initial polarization vectors.

$E_i = \begin{pmatrix} 1 \\ 0 \end{pmatrix}$  is  $P_{\text{vertical}}$ . We can drop the normalization factors in  $A$  and  $E_i$

i)  $E_t = \begin{pmatrix} 1 & i \\ i & 1 \end{pmatrix} \begin{pmatrix} 1 \\ 0 \end{pmatrix} = \begin{pmatrix} 1 \\ i \end{pmatrix}$  is  $P_{\text{vert}} \xrightarrow{A_1} L_{\text{state}}$

ii)  $\begin{pmatrix} 1 & i \\ i & 1 \end{pmatrix} \begin{pmatrix} 0 \\ 1 \end{pmatrix} = \begin{pmatrix} i \\ 1 \end{pmatrix} = \text{const} \begin{pmatrix} 1 \\ -i \end{pmatrix}$  is  $P_{\text{hor.}} \xrightarrow{A_1} R_{\text{state}}$

iii)  $\begin{pmatrix} 1 & i \\ i & 1 \end{pmatrix} \begin{pmatrix} 1 \\ -i \end{pmatrix} = \begin{pmatrix} 1+i \\ i-i \end{pmatrix} = \text{const} \begin{pmatrix} 1 \\ 0 \end{pmatrix}$  is  $R_{\text{state}} \xrightarrow{A_1} P_{\text{vert}}$

iv)  $\begin{pmatrix} 1 & i \\ i & 1 \end{pmatrix} \begin{pmatrix} 1 \\ i \end{pmatrix} = \begin{pmatrix} 1-i \\ i+i \end{pmatrix} = \text{const} \begin{pmatrix} 0 \\ 1 \end{pmatrix}$  is  $L_{\text{state}} \xrightarrow{A_1} P_{\text{hor.}}$

This is some combination of wave plates, i.e. it is some combination of multiples of Jones matrices. — I am not sure what combination but the characterization of the action of  $A_1$  is summarized i.e. i) thru iv) above.

8.71 b) Consider the action of  $A_2 = \frac{1}{\sqrt{2}} e^{i\pi/4} \begin{pmatrix} 1 & -i \\ -i & 1 \end{pmatrix}$

on various initial polarization vectors. Again we can drop the normalization factors

$$i) \begin{pmatrix} 1 & -i \\ -i & 1 \end{pmatrix} \begin{pmatrix} 1 \\ 0 \end{pmatrix} = \begin{pmatrix} 1 \\ -i \end{pmatrix} \text{ ie } \underline{P_{\text{vert}} \xrightarrow{A_2} R_{\text{state}}}$$

$$ii) \begin{pmatrix} 1 & -i \\ -i & 1 \end{pmatrix} \begin{pmatrix} 0 \\ 1 \end{pmatrix} = \begin{pmatrix} -i \\ 1 \end{pmatrix} = \text{const} \begin{pmatrix} 1 \\ i \end{pmatrix} \text{ ie } \underline{P_{\text{Hor}} \xrightarrow{A_2} L_{\text{state}}}$$

$$iii) \begin{pmatrix} 1 & -i \\ -i & 1 \end{pmatrix} \begin{pmatrix} 1 \\ -i \end{pmatrix} = \begin{pmatrix} 1-1 \\ -i-i \end{pmatrix} = \text{const} \begin{pmatrix} 0 \\ 1 \end{pmatrix} \text{ ie } \underline{R_{\text{state}} \xrightarrow{A_2} P_{\text{Hor}}}$$

$$iv) \begin{pmatrix} 1 & -i \\ -i & 1 \end{pmatrix} \begin{pmatrix} 1 \\ i \end{pmatrix} = \begin{pmatrix} 1+1 \\ -i+i \end{pmatrix} = \text{const} \begin{pmatrix} 1 \\ 0 \end{pmatrix} \text{ ie } \underline{L_{\text{state}} \xrightarrow{A_2} P_{\text{vert}}}$$

Thus the characterization of  $A_2$  is summarized in i) thru iv) above.